

RIGA TECHNICAL UNIVERSITY
Faculty of Civil Engineering
Institute of Transport Structures

Andris PAEGLITIS

**TRAFFIC LOAD MODELS FOR LATVIAN ROAD
BRIDGES WITH SPAN LENGTH UP TO 30 METERS**

Summary of doctoral dissertation

Civil Engineering „RTU P-06”

Supervisor
Dr. sc. ing, prof.
Ainars PAEGLITIS

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**DISSERTATION
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OFFICIAL OPPONENTS:

Prof. Dr.habil.sc.ing. Janis Brauns
Latvia University Of Agriculture
„RTU P-06” member

Dr. Assoc. Prof. Darius Bacinskas
Vilnius Gediminas Technical University
Department of Bridges and Special Structures

Doc. Dr.sc.ing. Kaspars Bondars
Riga Technical university

CERTIFICATION

I hereby certify that I am the author of the present dissertation, which is submitted for consideration at Riga Technical University for obtaining a Doctor's Degree in Engineering Sciences. The dissertation has not been submitted for obtaining a scientific degree at any other university.

Andris Paeglitis(Signature)

Date: 26.09.2012

The dissertation is written in the Latvian language and comprises an introduction, 8 chapters, conclusion, bibliography (82 sources) and altogether 115 pages.

REVIEW OF DISSERTATION THESIS

Topicality of the Dissertation Thesis

European Union (EU) transport policy is to "ensure high level of mobility to the people and businesses. Accessible and high-quality transport solutions for reasonable rates, free movement of persons, goods and services (within the functioning) that insure improved social and economic cohesion, and provides Europe industry competitive capacity"(EC commission communication & EC, 2006). Transport flow in Europe is dominated by the road transport and serves all Europeans on a daily basis. In the European Union 83% of the passenger traffic and 46% of all commercial traffic is being provided by roads.

To implement the EU's transport policy requires new knowledge and innovative solutions. Therefore, one of the EU's research priorities has become the research of road infrastructure network enhancement techniques (EC, 2008). Compared with previous years, new roads and bridges are being built less often, hence greater investment in maintaining the functioning of existing infrastructure is needed, moreover, to insure appropriate safety standard implementation. Over the past years the number of vehicles on EU roads has increased. From 2000 to 2008 the number of vehicles in the EU has increased 17% and 75% in Latvia and heavy traffic in the EU has increased 25% and 34% in Latvia (European Commission, 2010). This indicates continued growth of the traffic load and its composition changes, and has to be taken into account for both the design of the new bridges and evaluating existing ones.

Currently there are 936 bridges on the Latvian national road network, of which: 880 are reinforced concrete bridges, 16 are bridges of stone and brick, 33 are steel bridges and there are seven timber bridges. Most of the bridges have been built after the Second World War. Regular bridge inspections have shown that about 60% of the bridges in service have varying degrees of damage that affects their bridge load-carrying capacity. Bridge damage can be caused by deterioration of the structure, poor quality of materials and construction, lack of maintenance, increasing traffic loads and environmental pollution. Considering the current financial situation and with the limited amount of money dedicated to the necessary bridge reconstruction or repair, it is important to clarify the actual traffic load effect on the bridge structure, to evaluate its structural capacity and determine the limits within which the existing bridge structures are safe to operate.

Bridge design in Latvia is based on Eurocode LVS EN 1991 Part 2 "Traffic load for bridges" where traffic load model LM1 is used. This model was derived in the late eighties when calibration of the heavy traffic loads was done. Data used for this model were obtained in France by two weeks of counting vehicles on the road A6 Paris - Lyon. Safety of a new structure increases because of its new materials with greater performance, improved quality of the execution and development of analytical and numerical methods of the structural analysis. For safety assessment of in-service bridges, the general approach given in Eurocode is being used. However, suitability of this approach for older bridges gives unreasonably low load carrying capacity, because it considers traffic load models and material characteristics devised for new structures. At the same time the actual traffic load and actual bridge structure material characteristics can vary considerably.

Until now determination of the traffic loads was a long and time-consuming process during which the road traffic was counted and vehicles weighed in specified locations. The obtained data were then used for traffic load forecasting. This collected data was not always sufficient and accurate; however according to them normative load models of the bridge design were developed.

In recent years new methods have been developed which with reasonable accuracy allow determination of the actual traffic load, traffic composition and intensity on the existing bridges. One of such methods is „weight in motion "(WIM), which will be used in this study. This method uses a measurement system, which allows measurement of gross weight, axle load, axle number and speed of each vehicle in motion.

Bridges and overpasses on Latvian roads have been built at different times, under various regulatory traffic load models, different requirements for building materials and construction technologies, but they all must be equally safe during service life. Bridges are permanent structures with service life often more than 100 years (Paeglitis, An., Paeglitis, Ai., 2012). Latvia started to use normative load models for bridge design in 1900. During the past century, load models changed more than six times, and each time vehicles gross weight has been increased, thus every load model is taken into account in the design of new bridges. With increasing knowledge of structural behavior design calculation methods have become more and more precise. Therefore, it is possible to reassess bearing capacity of existing bridges by applying modern transport load models. Load models given in Eurocodes often give larger stresses than the original load model of an "old" bridge, therefore bearing capacity is evaluated as insufficient. Although the load-bearing capacity is not sufficient for the Eurocode load models, it is adequate for the actual traffic load.

It is therefore important to identify and analyze the actual traffic load obtained from WIM system and develop a specific Latvian road traffic load model for in-service bridge bearing capacity assessment.

Objective of study

Develop Latvian road traffic characteristic load models for bridges with span lengths up to 30 meters, using data provided by the "weight in motion" method obtained from a device on motorway A4 (Baltezers - Saulkalne) and analyzed using a probability-based analysis methods.

Identify specific types of vehicles most often found on Latvian roads, as well as to determine LVS EN 1991-2 Eurocode load model LM1 given regulatory factor α recommended values for existing bridge carrying capacity assessment, taking into account determined new traffic load models.

Task of the study

- Evaluate the earlier studies on the traffic load modeling techniques that are based on WIM system to determine load bearing capacity of bridges. Analyze and evaluate historically used traffic loading models on bridges in Latvia.
- Develop a method based on statistical analysis and probability theory for calculations and simulations of typical traffic axle loads and the geometric parameters, frequency and non-existing probability distribution of the design parameters, the determination of the correlation between a given gross weight, number of axles and the geometrical parameters.
- Identify typical traffic load characteristics of Latvia using WIM data collected from the device on motorway A4 (Baltezers - Saulkalne).
- Develop Latvian road characteristic traffic load models for the bridges with span length up to 30 meters taking into account characteristic traffic loads.
- Determine LVS EN 1991-2 Eurocode load model LM1 given regulatory factor α recommended value taking into account characteristics traffic loads in Latvia.

Scientific novelty of the Dissertation Thesis

- Develop Latvian road characteristic traffic load models for the bridges with span lengths up to 30 meters taking into account their characteristic traffic loads.
- Develop a method based on statistical analysis and probability theory for calculations and simulations of typical traffic axle loads and geometric parameters, frequency and non-existing probability distribution of the design parameters, as well as determining the correlation between a given gross weight, number of axles and geometrical parameters.
- Identify traffic load characteristics on Latvian roads.
- Determine LVS EN 1991-2 Eurocode load model LM1 regulatory factor α recommended value taking into account characteristic traffic loads in Latvia.

Practical application of the Dissertation Thesis

Developed method based on probability theory and statistical analysis for processing WIM data to obtain typical traffic load characteristics of Latvia.

Developed Latvian traffic characteristic load models for bridges with span lengths up to 30 meters. The obtained results allow optimization of the bridge management system and increases safety on Latvian roads. Developed traffic load models can be used by the bridge keepers of LSR "Latvian State Roads" or municipalities to make adequate decisions in the bridge design and maintenance, thus saving public funds.

- Determined that LVS EN 1991-2 Eurocode load model LM1 regulatory factor α recommended value should be included in LVS EN 1991-2 National Annex of existing bridge carrying capacity assessment.

Results presented for defence of Dissertation Thesis

- Typical Latvian road traffic load characteristics were obtained using WIM data.
- Developed specific Latvian road traffic load models for bridges with span lengths up to 30 meters taking into account the characteristic traffic loads.
- Developed a method for processing traffic data loads based on statistical analysis and probability theory to determine the actual traffic load, load distribution between vehicle axles, cumulative gross weight and axle load distribution of the vehicle.
- Determined LVS EN 1991-2 Eurocode load model LM1 regulatory factor α recommended value taking into account the characteristic traffic loads in Latvia.

Volume of the Dissertation Thesis

The doctoral thesis consists of 8 chapters; thesis contains 115 pages, 119 figures, 37 tables, 82 literature sources.

Approbation of the work and publications

Thesis has been published in scientific journals and discussed at international conferences:

Publication in scientific journals, cited in SCOPUS database:

1. Paeglitis An., Paeglitis Ai., Vitina I., Igaune S. (2012.) Study and renovation of historical masonry arch bridge, *The Baltic Journal of Road and Bridge Engineering*, (accepted for publication).

The publication of scientific books, cited SCOPUS database:

2. Paeglitis An., Paeglitis Ai. (2012.) Investigation and upgrading of a historical multispan masonry arch Bridge. In: Biondini, F., Frangopol, D. and M. (Eds). *Bridge Maintenance, Safety, Management, Resilience and Sustainability*. Taylor & Francis Group, London, 1086-1093.p.

Publication in scientific journals, cited in EBSCO database:

3. Paeglitis An., Paeglitis Ai. (2010). Simple classification method for the capacity rating Bridge, RTU scientific articles. *Būvzinātne (Construction science)*, Series 2. Volume 11th: 44-50.
4. Paeglitis An., Paeglitis Ai., Cācis, R. (2012.) Weight-motion data in the analysis of vehicle loads of A4 motorway in Latvia, RTU scientific articles. *Būvzinātne (Construction science)* 2.Series 13th Volume 33, page 41 ..

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5. Paeglitis An., Paeglitis Ai. (2009.) Restoration of masonry arch bridge over river Venta in Kuldīga, Abstract Book, 27. International Baltic Road Conference, Riga, 2009, 24th - 26 August, page 6.
6. Paeglitis An., Paeglitis Ai. (2010.) Simple classification method for the capacity rating Bridge, RTU 51st International Scientific Conference, Riga, October 13, 2010 ..
7. Paeglitis An., K. Gode, Straupe V., Paeglitis Ai. (2011.) Traffic load analysis of the composition and intensity of the Latvian bridges, Joint World Latvian Scientists III. Congress "Science, Society and National Identity," section "Technical Engineering" Abstract Book, 2011 24 to 27 Oct., Riga, p.1.
8. Paeglitis An., Paeglitis Ai. (2012.) Investigation and upgrading of a historical multispan masonry arch Bridge, Proc. of 6th International Conference on Bridge Maintenance, Safety and Management (IABMAS 2012), Stresa, Italy, July 8-12, 2012, P 8.

CONTENTS OF THE DISSERTATION

The first chapter explains the topicality of the dissertation, sets the tasks and objectives, and formulates the results presented for the defence of dissertation, scientific novelty and practical application.

The second chapter is a brief analysis of previous studies. Traffic load is one of the most complex variables that significantly affect the uncertainty of the bridge element assessment. Traffic load models in different national standards are very conservative and are intended primarily for the design of new structures. Most of these models have been developed using a short time observation of heavy traffic flow on which long-term load effects are extrapolated. The resulting traffic load models for bridge design is based on the bending moment values in mid-span, but these models are not sufficiently precise for other stresses (eg, shear). Traffic load induced effects depend on many variables such as the vehicles weight, axle weight, axle spacing, speed, etc. .. Probability methods were used in the development of traffic load models that take into account various random variables.

"Weight in motion" (WIM) technology allows collection of precise information on the composition of the traffic flow which allows the modeling of traffic loads on bridges. Many authors in their papers show that the WIM data allow for fatigue prediction based on the actual traffic composition. These studies show the effectiveness of WIM data compared to other data collection methods, such as the stopping and weighing vehicles on the roadside. WIM technology is economically viable as it automatically collects data and does not require operating personnel, thus reducing the cost of data collection procedures. Prior study results show that by using WIM technology it is possible to obtain an objective description of traffic statistics and more accurate traffic load models. However, obtained traffic load models are specific to a particular country and it is not recommended to apply them for a bridge bearing capacity evaluation anywhere else.

In-service bridge carrying capacity assessment methods are based on the technical assessment and real-time traffic analysis of structures. Various studies show that the actual traffic load is up to 50% less than those in standards. Due to traffic loads given in national standards, we could design a bridge with a large carrying capacity margin, which sometimes is not economically viable. By studying the regulatory load factor α value, it is found that it is largely dependent on both the bridge span length and width of the roadway and the road category.

As the composition of traffic and assessment of each country is different and can not be used directly elsewhere, it is necessary to determine appropriate load models for Latvia using long-term WIM data.

Further analysis of historical and currently used traffic load models for bridges in Latvia and their load value increases was performed. It was found that vehicles used today, compared to those historically used, are longer, with a higher number of axles and the larger distance between them, so their effect on the load bearing construction of the bridge in many cases will be smaller as all axles can not fit onto a small or mid-span bridge at the same time. Therefore, it is important to clarify typical traffic load patterns of Latvian road bridges and integrate them into the small-and medium-span bridges carrying capacity assessment of existing bridges.

In **the third chapter** the method develops an analysis of the data traffic load, using WIM data.

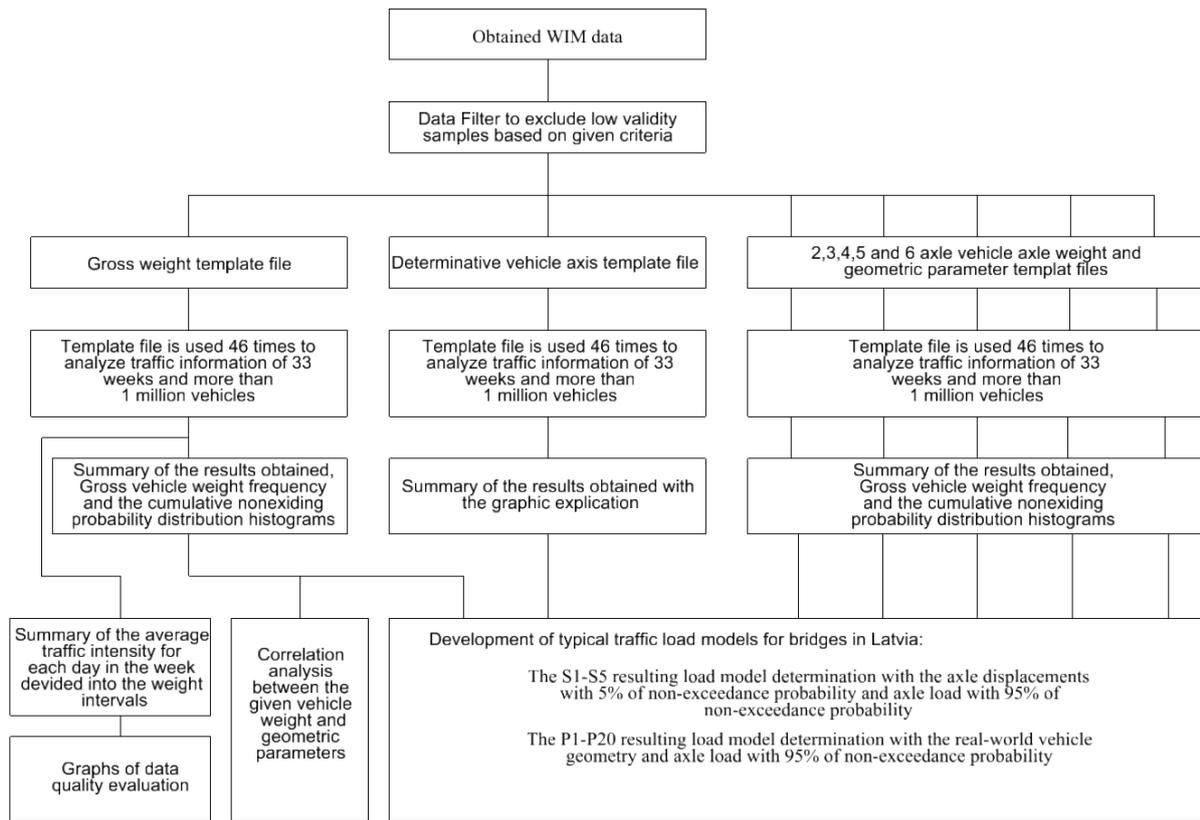


Fig.1. Flowchart of traffic load analysis method

Part of the WIM data had to be excluded from further processing due to low validity. Data exclusion was done using (A. Pratt, 1998) study given criteria:

- The first criterion is the maximum permissible axle load, which was adopted equal to 40 tons.
- The second criterion is the total weight maximum of the vehicle, which is assumed equal to 300t.
- The third criterion requires a minimum total vehicle weight of 3.5 t. In this way only heavy vehicles are taken into account.
- The fourth criterion is the speed of the vehicle. Its limit is set at 150 km / h. It is more than the permitted speed limit. However, due to vehicle drivers reckless driving much of the heavy vehicles data would not be included

The next step in data processing is establishment of the template file for each set of parameters. The first template file includes information on all of the axles weight distribution, the maximum axle weight distribution, distributed load distribution and gross vehicle weight distribution of 2,3,4,5,6, and > 6-axle vehicles. The second template file was created to evaluate determinative vehicle axis and total number of vehicles divided by the number of axles. The third, fourth, fifth, sixth and seventh template file is created similar to that described above, the only difference is number of axles, which, accordingly, are accepted 2, 3, 4, 5 or 6. In processing of the data, 46 files was created that contained information about 1 million vehicles. In each data file complete traffic information of 33 weeks was utilized creating in total 322 processing files.

This chapter explains the main methods of statistical analysis and probabilities based calculation and simulation methods for vehicle axle loads and geometrical parameters selection to create the traffic frequency and cumulative distributions, and to determine the correlation between these geometric parameters. It is also used for final load model determination.

For the selection and representation of geometrical parameters the frequency and cumulative distributions histograms are widely used. For histogram design, the following algorithm was used. The variable number n was determined for every measured value that reached one million, and range r depends from the measurements maximum and minimum values (Kronberg, 1988). Both the number and size of variable classes in this research were determined according to necessary accuracy. The total axle loads and maximum axle load distribution load class size was adopted - 0.2 t, and distributed load - 0.2 t / m, while vehicle gross weight distribution class size was equal to 1t. For individual 2, 3, 4, 5 or 6 axle vehicles weight and axle placement parameters were defined following class sizes: speed distribution - 5 km / h, vehicle length - 0.5m, axle load distribution - 1t, and axle separation distribution - 0.5m. When vehicle load models P1 - P20 were created a class size of distance between the axles was reduced to 0.25m.

Absolute class frequencies n_j is calculated next by counting how many random elements are in each class interval. To select and count the number of elements within each class of variables MS Excel function "COUNTIF" were used in. The relative class frequency f_j can be determined by dividing the absolute frequency of class N_j with the total number of elements in the sample n (1.1).

$$\sum_1^{n_c} f_j = 1 \quad (1.1.)$$

The absolute class cumulative frequency is N_j . Variable class j is the total number of elements that fall into the classes from $N_1 = 1$ to $N_i = j$ inclusive. The relative cumulative frequency of class F_j is obtained by dividing the absolute cumulative frequency of the class N_j and the total number of elements in the sample, N . If $j = n_c$, then $F_j = 1$, formula (1.2.).

$$F_j = \frac{N_j}{N} \quad (1.2.)$$

The resulting values are summarized in the table and are designed as based on the data table histogram.

In cases where it is practically impossible to calculate probability in the classical definition, the relative frequency calculated for a large number of attempts can be used instead. (Kronberg, 1988) This means that the greater the amount of collected data, the more accurately it describes the probability values. Based on the large amount of data used in this study it is assumed that the relative cumulative frequency graph values represent necessary probability.

The fourth chapter describes the WIM technology advantages and weaknesses for data acquisition and discusses the quality of data collected.

For this study used WIM data were obtained from measuring equipment which was installed from year 2002 to 2008 on the motorway A4 (Baltezers - Saulkalne) between P5 and A6 (Riga - Daugavpils - Kraslava-Belarus border (Pāternieki)). The measuring equipment was located 500 meters before intersections in this roadway, thus providing free traffic conditions and a good data collection situation. In 2011 the measuring equipment was dismantled because the sensor was damaged by the traffic load.

Within six years WIM system collected data on more than 17,568,000 vehicles, about 244 000 vehicles a month. Initial processing of the data showed that the WIM sensor error in the first year was about 5% in the second year - 15% and in third year 25%.

Data from year 2002 and 2003 were not used in this reaserch because of its very fragmentary nature, but the 2005 - 2008 data was already of poor validity and were excluded from further processing. Therefore, this study was carried out by processing only data from year 2004 that consisted of 33 weeks of measurements. Total magnitude of vehicles in 2004

was 1,172,842. Of these, 449,218 vehicles weighed less than 3.5 tons, but 663,101 vehicles weighed more than 3.5 tons. Data on 60,523 vehicles were incomplete and could not be used for further analysis. Statistical analysis of data showed that 861,165, or 79.82% are two-axle vehicles. The second largest group was the five-axle vehicles – 12.48%, and three-, four- and six-axle vehicles were only 6.25% of the total.

In order to evaluate the proportion of heavy vehicles in traffic, it was decided to divide it into three groups:

- light vehicles, weighing up to 3.5 t
- heavy vehicles, weighing from 3.5 tons to 20 tons,
- very heavy vehicles, weighing from 20 tons to 300 tons.

The data shows that the light vehicle traffic portion is about 41% of total, 39% is heavy and 20% very heavy vehicles. Given that the number of vehicles is dependent on the day of the week, each group of traffic were fitted into graphical Figure 2.

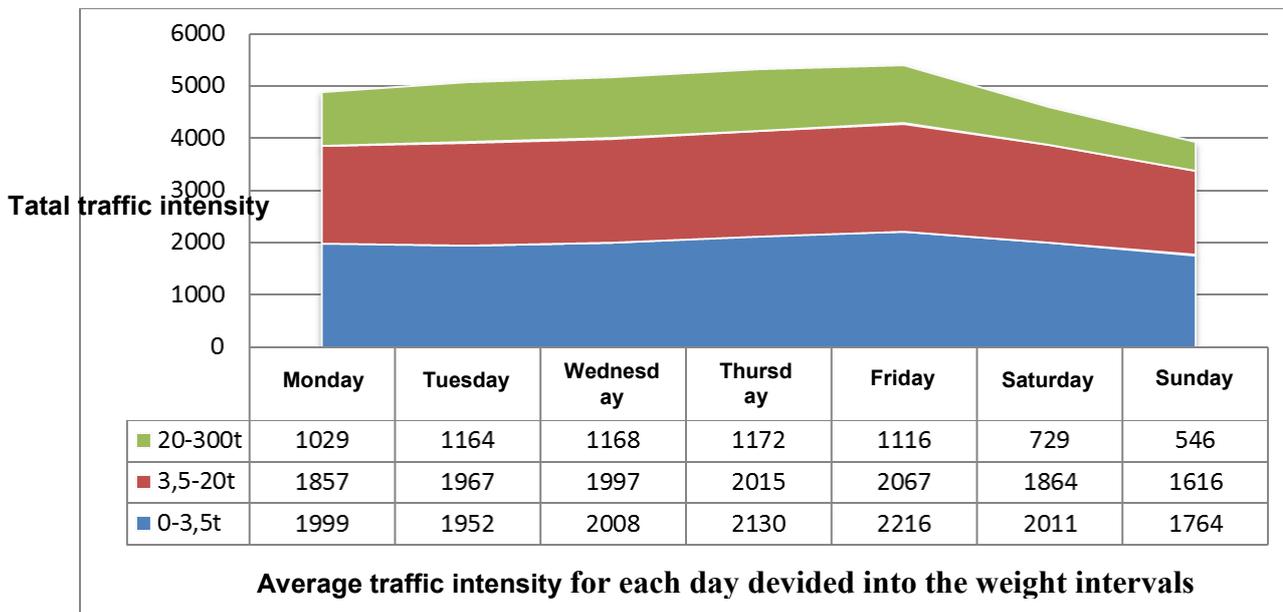


Fig.2. The average traffic intensity of year 2004 for each day in the week divided into the weight intervals 0-3.5t, 3.5- and 20-20t 300t

The results show that the intensity of traffic on the Latvian road depends on the day of the week, peaking in Tuesdays and Fridays. This tendency remains in four weeks, three months, six months, as well as in twelve months period. Knowing the intensity maximums and distribution of heavy vehicles, it is possible to plan and coordinate new data collection of intensity or weight, as well as organizing construction or reconstruction road work.

Analysis of the used data shows that the quantity of valid data is 1,078,403 vehicles and tendency of intensity is stable which ensures adequate results. This provides a good basis for a comprehensive analysis of the traffic load.

The fifth chapter represents the results of WIM data analysis. It is determined Latvia-specific road traffic load characteristics generated load distribution histograms that determined the heaviest axle positions, analysed correlation between speed and intensity and defined which probability distribution function shapes correspond to the load distribution histograms.

Analysis of Gross vehicle weight showed that the largest proportion of vehicles on the roads are cars with a mass around 3.5 t, the second largest proportion of vehicles weigh around 37 tons, while the third - with a mass of 90 t (Figure 3). The maximum vehicle weight

of 94-95t is determined with 95% probability, with the remaining 5% of vehicles with a mass of up to 300 tons occur very rarely and must receive special permits from authorities.

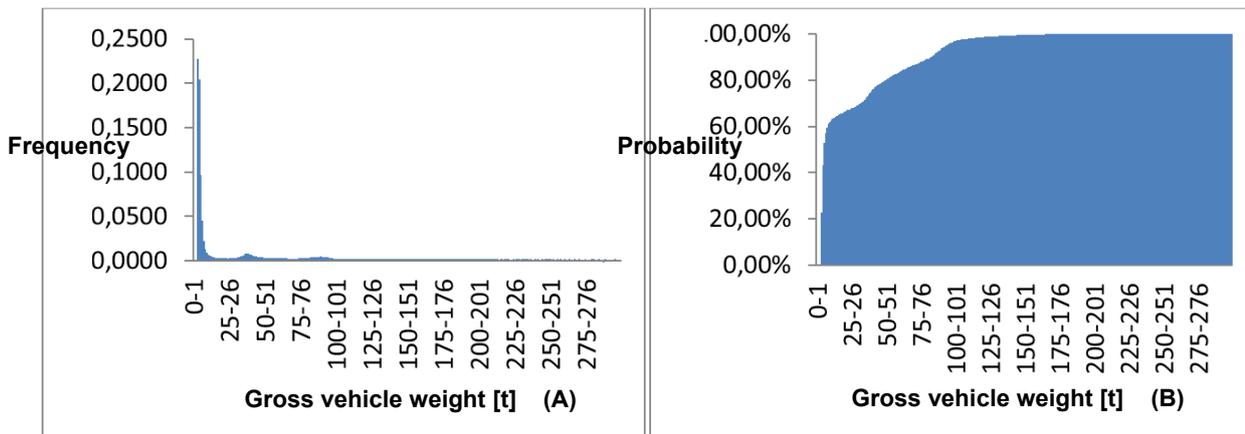


Fig.3. Gross vehicle weight frequency (A) and the cumulative nonexiding probability (B) distribution

Vehicle distribution by number of axles showed that most, around 67% on the Latvian roads are two-axle vehicles that represent passenger cars and light commercial vehicles, the second largest group with 21% is five axle vehicle trucks - lorries, and the third group is four-axle vehicles that constitute approximately 5% of the total traffic (Figure 4).

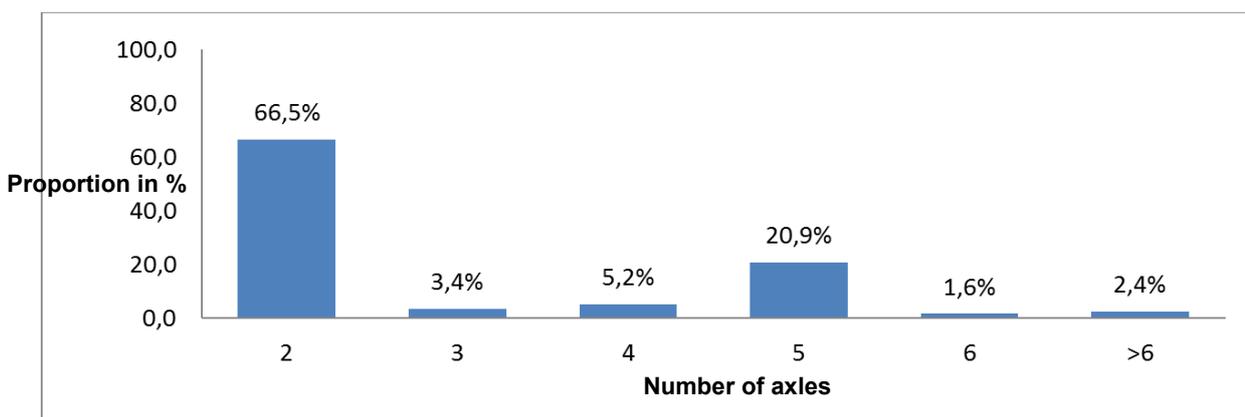


Fig.4. Proportion of vehicles divided by number of axles

At the same time, in the analysis of two axle vehicles, it was found that in approximately 70% of cases the heaviest are the first axle. Usually though, it is assumed that the rear axle is the heaviest, but that is only in the case when the vehicle is loaded to the permissible level. This outcome is explained by the fact that heavy vehicles are often partially empty. A large part of a two-axle vehicles around 3.5 t are cargo vans, which carry a variety of items, but the weight of the goods is usually not sufficient to make the second axle the most heavy one. A similar situation exists in three-axle vehicles, where the heaviest axle turns out to be the first and second axle. For four, five and six-axle vehicles statistically the heaviest is the second axle. Thus it can be concluded that the statistically heaviest is not always the last axle, as assumed in many load models assessed before 1984. This means that checking the load carrying capacity of the bridge must take into account the uneven distribution of axle load.

In researching actual vehicle geometry (length and axis placement), data were derived on the statistically most frequent vehicle length and axle placement. The results pointed to a large variety that must be taken into account when defining the load models.

By studying the mass and axle weight distributions, it was found that the two-axle vehicle first and second axle weight distributions are similar shape of normal distribution (an example is given in Figure 5).

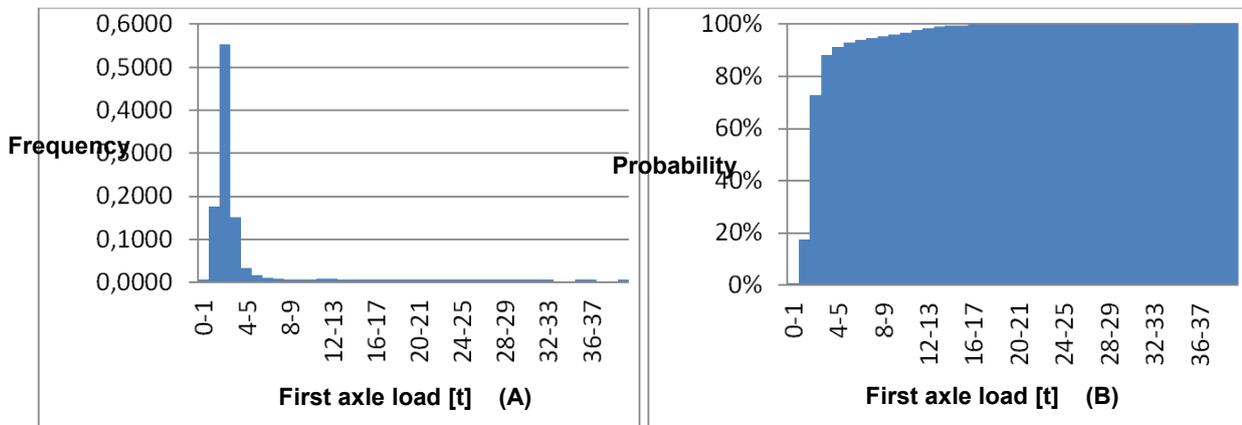


Fig.5. Two-axle vehicles first axle load frequency (A) and the cumulative nonexiding probability (B) distribution

In three, four, five and six-axle vehicles the mass frequency distribution is dominated by a bimodal shape, an example is given in Figure 6.

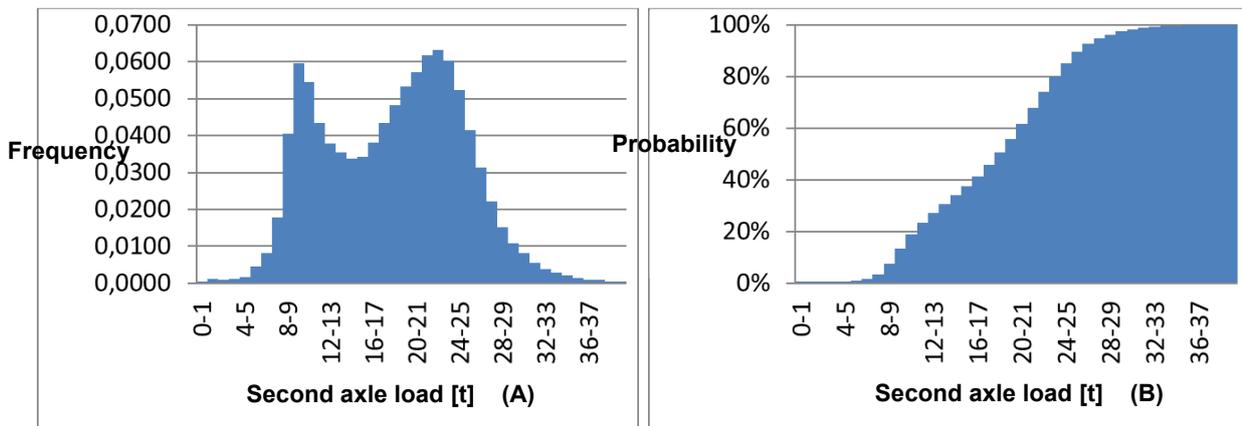


Fig 6. The five-axle vehicles of the second axle load frequency (A) and the cumulative nonexiding probability (B) distribution.

This type of the weight distribution shape indicates two possible cases – first, the movement of loaded and empty vehicles and second, that there are two separate distinctive types of vehicles. Checking the geometric parameters, two distinctive types of vehicles have not previously been identified. Thus, bimodal distributions with the first peak less disperse than the second clearly indicates the first case (above). It should be noted that the weights depend on many factors, such as a fullness of petrol tank, number of passengers, etc .

To find whether the interrelations between the traffic data exist, the correlations are analyzed. If an interrelation is found, it is measured by the correlation coefficient and if the relationship is close or positive, then with certain accuracy it is possible to determine one value expressed with another. This can be useful as data collection of weight of the vehicle is very expensive and complex.

The mathematical model or regression equation is applied that represents relationships between variables in chart Figure 7. The regression curve can be linear or non-linear and to find the most accurately expressed regression equation four possible options are evaluated: exponential, linear, logarithmic, and polynomial. The most appropriate equation is chosen by analyzing the highest value of determination coefficient R^2 .

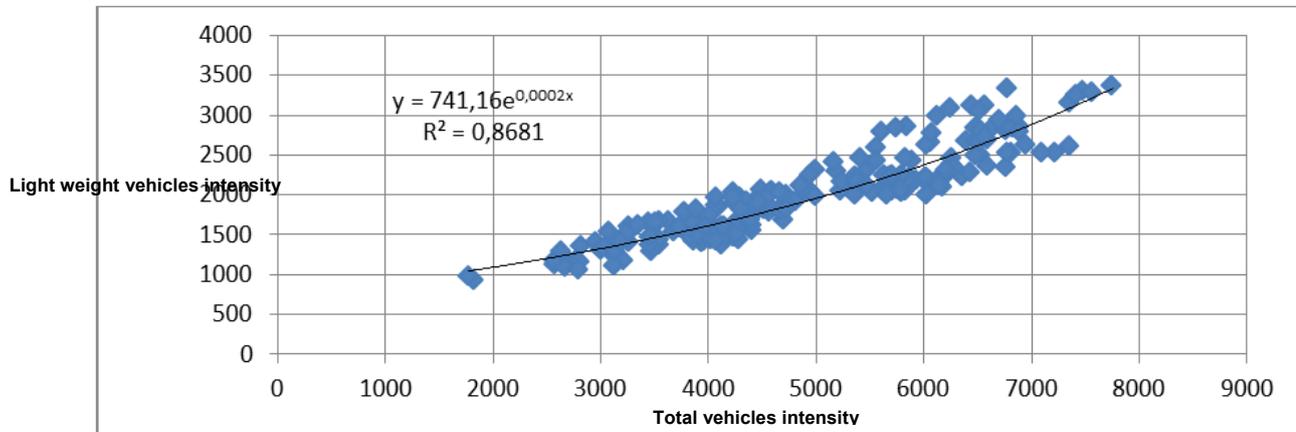


Fig.7. Correlation between total and light weight vehicles intensity

The relationship between total and light weight vehicles intensity shows a strong correlation with a coefficient of determination $R^2 = 0.8681$. Mathematical model equation is exponential and it is expressed by the formula (1.4).

$$y = 741.16 * e^{0.0002x}. \quad (1.4)$$

Similarly the correlations are obtained between the total and the heavy traffic intensity, heavy and light vehicles intensity, and so on.

Acquired relationships allow you to restore the traffic load values using data on traffic intensity and heavy and light vehicles relations.

The sixth chapter represents the developed and analyzed typical traffic load models for bridges in Latvia, using defined typical bridge construction types in Latvia. The effects on different span lengths were studied, including simply supported beam and continuously supported beam system bridges. The three most important characteristic traffic load models in Latvia were identified.

Traffic load is a variable which can not be directly modeled, but the use of statistical methods makes it possible to gain reliable data on traffic load values. Based on (LVS_EN_1991-2_NA, 2004) the load model LM1 calibration can be done using traffic loads of the repetition period of 1000 years, or a 5% of exceedance probability in 50 years. This means the non-exceeding probability of 95%.

In this study in order to find the critical traffic load models two approaches were proposed.

The first approach is directly related to the fifth chapter of thesis where geometric and load parameters were defined. The resulting load models consist of the axle displacements with 5% of non-exceedance probability and axle load with 95% of non-exceedance probability. The 5% non-exceedance probability is needed to describe the minimum possible distance between the axles.

From the resulting parameters load, models S1 - S5 have been developed as shown in Figure 8.

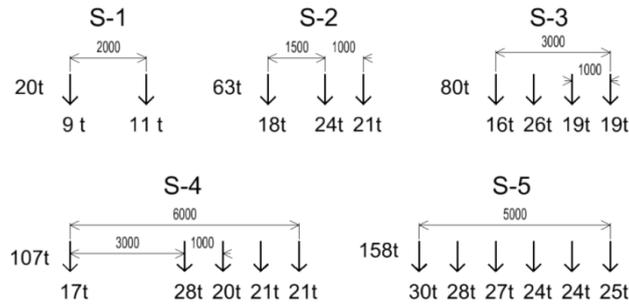


Fig.8. Vehicle load models S1-S5

The resulting values are conservative, because it takes into account the distances between all types of vehicle axles and only the heaviest axle weight with non-exceedance probability of 95% (which is unlikely) are fitted in model. It is almost impossible to identify, but only the heaviest axle load within the range falls below 95% probability. However it covers great uncertainty and guarantees the safety and validity.

The second approach involves real-world vehicle geometry analysis. Specific types of vehicle geometry were obtained by further analysis of the traffic composition, based on the axle displacement distribution histograms. Since some axle displacement frequency histograms were with two or three peaks, there was an additional assessment done to the data and they were broken down so that each peak represents single truck geometry.

The results created loads models P-1 to P-20, given in the Figure 9 and Figure 10.

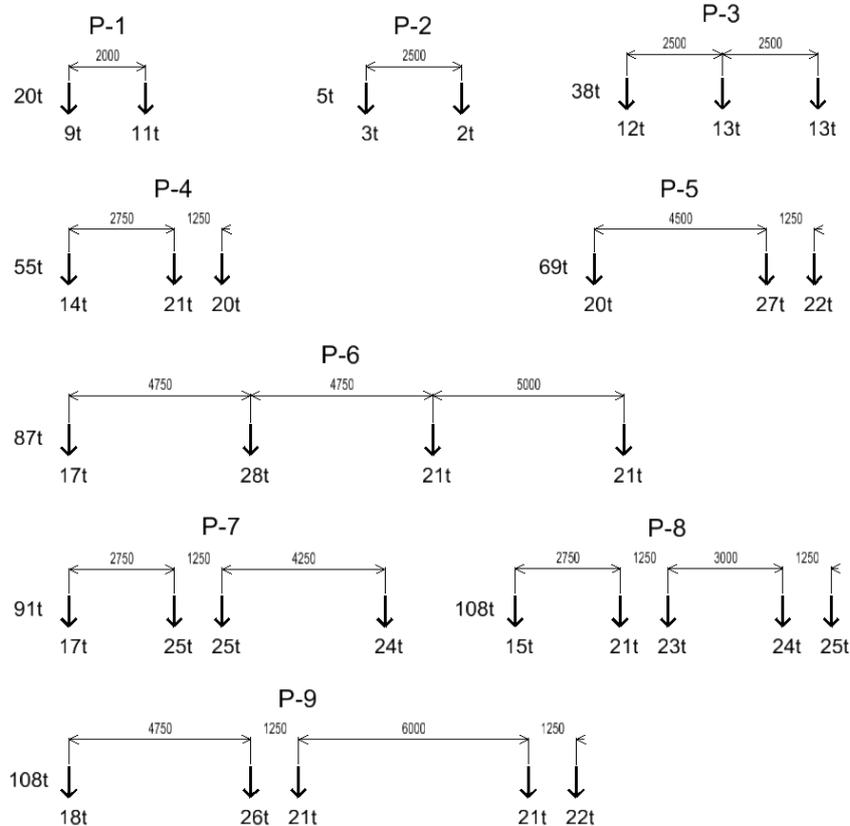


Fig.9. Traffic load model P-1 to P-9

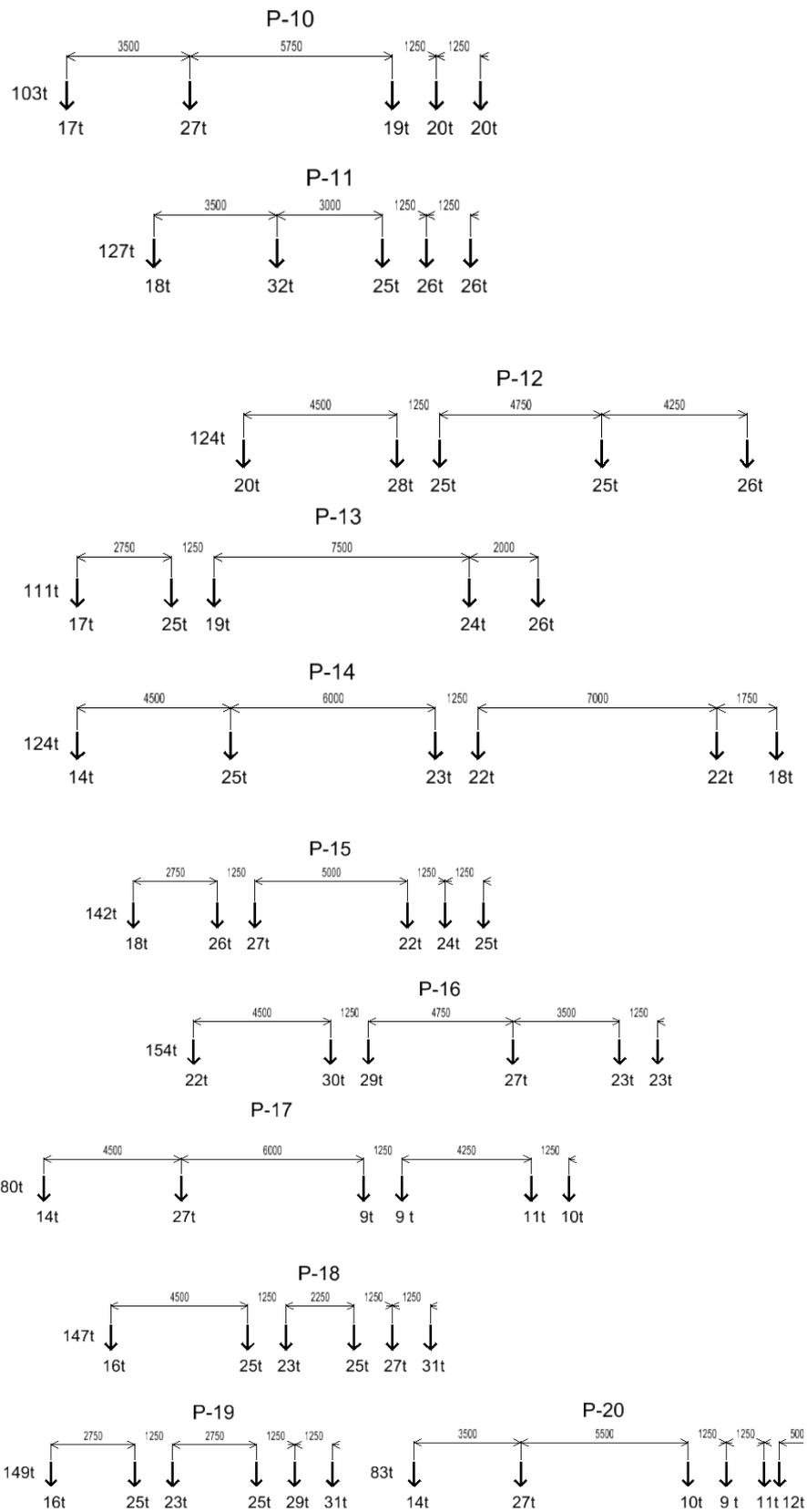


Fig.10. Traffic load model P-10 to P-20

To determine the range of the bridges which will be affected by the new traffic load models the investigation of Latvia characteristic span structure types were done. Using VAS "Latvijas Valsts Ceļi (Latvian State Roads)" bridge management system and taking into account the typical bridge span lengths, for the calculations of simply supported beam system bridges span lengths are taken as follows: 6, 9, 12, 15, 18, 21, 24 and 33 meters, while the three-span continuously supported beam system bridges span lengths are 9 +12 +9, 12 +15 +12, 15 +18 +15, and 18 +24+18.

To determine which of the new traffic load models: S-1 to S-5 and P-1 to P-20 will inflict the largest effect, the simply supported beams bridge with the span lengths of 33, 24 and 21 m were tested using computer program Dlubal RFEM 4.05 which is based on the finite element method. A design model of bridge was made with the 9 m wide deck and two 1.5 m wide pavement on each side. The thickness of span construction was 2 m to minimize the impact on the deflections. The dead load was not included in this assessment. To replicate pedestrian load together with load models: S-1 to S-5 and P-1 and P20 the 3 kN/m² of distributed load were placed on the sidewalks. Traffic load models are placed on the left side of the deck. The first wheel of the axle is 0.5 m from the edge of the deck and the distance between the wheels on one axle is 2 m. In order to establish the less favorable load distribution, the impact-line diagram is used.

Placing a load models on the bridge structure the maximum bending moment M1 and shear force Q2 values are obtained. All-span structure is also loaded with LVS EN 1991-2 load model LM1 where regulatory factor $\alpha = 1$.

Based on the results the worst possible effect on the bridge span was achieved from traffic load models S-5, P-18 and P-19 (Figure 11). Consequently, these traffic models are recommended for use when inspecting the bridge bearing capacity in Latvia.

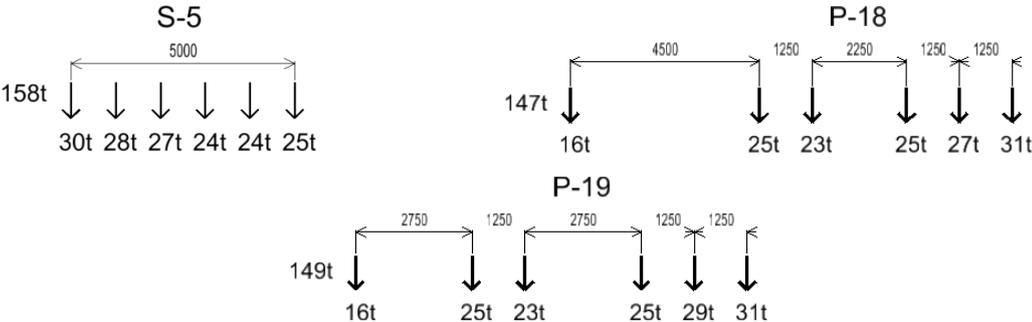


Fig.11. Latvia typical load models S-5, P-18 and P-19

- In order to simplify the application of the developed load models, they are renamed:
- S-5 to LSM1 with a total weight of 107 tons and geometry given in Fig.11.
 - P-18 to LSM2 with a total weight of 147 tons and geometry given in Fig.11.
 - P-19 to LSM3 with a total weight of 148 and geometry given in Fig.11.

Obtained load models significantly exceed the permitted load limits on the roads. However, analyzed traffic data showed that these traffic models are possible on Latvian roads.

The seventh chapter represents the determined regulatory factor α recommended values for Eurocode LVS EN 1991-2 load model LM1 given regulatory factor α recommended value for existing bridge carrying capacity assessment in Latvia.

Eurocode allows that each Country in its National Annex document can regulate the traffic load values, according to the country-specific traffic loads through regulatory factor α .

Load regulatory factor may be determined by the bending moment and the shear force using LM1 load model (with $\alpha = 1$), with are compared with Latvia typical traffic load models LSM1, LSM2 and LSM3 obtained in Chapter 6.

The results show that regulatory factor α value of continuously supported beam structures is less sensitive to span lengths than simply supported beam structures and vary from 0.58 to 0.82.

Based on the results, the regulatory load factor α can be calculated in range from 0.51 to 0.87, by taking into account the type of structure and the span length. The biggest effect on the structures was from load model LSM1.

Since regulatory factor values depend on the length of the span, two intervals can be identified: from 6 m to 18 m and from 18 m to 33 m, and for each interval regulatory factor α value are determined. Recommended values are summarized in Table 1.

Table 1.

The recommended regulatory factor α_{Qi} , α_{qi} and α_{qr} values for bridges with spans up to 30 m

Laidumu intervāls	α_{Qi}	α_{qi}	α_{qr}
6 – 18 m	0.8	0.8	0.8
18-30 m	0.9	0.9	0.9

Acquired regulatory factor α_{Qi} , α_{qi} and α_{qr} values are close to those given in the National Annex 2 of 1.Eirokodeksa, but they are about 10% smaller. Using the regularization coefficient α values can accurately assess the load carrying capacity of the bridge, and make reasoned decisions about bridge construction or renovation, thus reducing the cost of surface transportation infrastructure maintenance.

The Eighth chapter presents the main conclusions that can be found in the next chapter summary.

CONCLUSIONS

1. Eurocode LVS EN 1991-2 "Traffic load bridges" load model LM1 (with a regulatory factor $\alpha = 1$) is designed for new construction and gives an unreasonably low load carrying capacity for older bridges. Therefore, using typical Latvian road traffic load characteristics, obtained by measuring weight in motion (WIM) and using the new modeling method, the numerical traffic load models LSM1, LSM2 and LSM3 are established. These allow more accurate assessment of bridge load-carrying capacity and reduction of bridge structure maintenance costs. The developed method makes it possible to calibrate the developed traffic load models and update them as new data are received and processed, as well as adjust the traffic load model according to traffic load changes.
2. Accuracy of the developed traffic load modeling method depends on the amount of experimental data. In order to characterize the actual traffic load and geometric parameter values non-exceeding probability of 95%, it is necessary to analyze traffic observation for at least 30 weeks, which coincides with the minimum data required for the use of method. If the amount of data increases the method becomes more accurate.
3. Determined correlation coefficients allow updating of traffic load values using measurements of traffic intensity and the relationship between heavy and light weight vehicles.
4. By applying load models LSM1, LSM2, LSM3 on bridges with span lengths up to 30 m and with a width of two lanes, resulting stresses are reduced by up to 20% compared to Eurocode LVS EN 1991-2 load model LM1 (with $\alpha = 1$), because load models LSM1, LSM2 and LSM3 characterize actual Latvian traffic load obtained by the WIM system. Bridges with greater span length and width require different load models.
5. When considering stresses created under load model LSM1, LSM2 and LSM3 on bridges with span lengths up to 30 m and width of two lanes, LVS EN 1991-2 Eurocode load model LM1 produces a regulatory factor α recommended value that can be decreased to $\alpha = 0.8$ for span lengths from 6 m to 18 m and $\alpha = 0.9$ for span lengths from 18 m to 33 m. This allows design of more cost efficient new structures.

