

RIGA TECHNICAL UNIVERSITY
Faculty of Power and Electrical Engineering
Institute of Power Engineering

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“Power and Electrical Engineering”

**A NEW DESIGN OF M.V – VACUUM CIRCUIT
BREAKER – WITH AUXILIARY UNITS DAMPING
TECHNIQUES FOR SOFT INTERRUPTER
APPLICATIONS**

Summary of the Doctoral Thesis

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DOCTORAL THESIS PROPOSED TO RIGA TECHNICAL UNIVERSITY FOR THE PROMOTION TO THE SCIENTIFIC DEGREE OF DOCTOR OF ENGINEERING SCIENCES

To be granted the scientific degree of Doctor of Engineering Sciences, the present Doctoral Thesis has been submitted for the defence at the open meeting of RTU Promotion Council on December 9, 2019 14.00 at the Faculty of Power and Electrical Engineering of Riga Technical University, 12 k-1 Azenes Street, Room 212.

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DECLARATION OF ACADEMIC INTEGRITY

I hereby declare that the Doctoral Thesis submitted for the review to Riga Technical University for the promotion to the scientific degree of Doctor of Engineering Sciences is my own. I confirm that this Doctoral Thesis had not been submitted to any other university for the promotion to a scientific degree.

Shaker Jassem Gatan (signature)

Date:

The Doctoral Thesis has been written in English. It contains 3 chapters; conclusions; 79 figures; 5 tables; 4 appendices; the total number of pages is 105. The Bibliography contains 118 titles.

CONTENTS

GENERAL DESCRIPTION OF THE WORK	5
Topicality	5
Technical engineering specification	5
Object of the Research	6
Aim and Tasks of Research	6
Tasks of the Thesis	7
Applied Research Methods	8
Scientific Novelty of Research	8
Scientific and Practical Approbation of the Work	9
Innovations	10
Author's publications	11
 STRUCTURE OF THE WORK	 13
1. Medium Voltage Switching Parameters	13
2. Contacting Materials of M.V Switching	13
3. Design Circuit & Mathematical Applications	13
 DISSERTATION BRIEFLY	 14
 I. FABRICATING AND DESIGNING	 16
1. HYPOTHESIS OF STATIC VACUUM INTERRUPTER	16
1.1. Designing, fabricating and modifying of the Petersen Reactor	
Coils Automatic Tuning	17
1.1.1. Fabricating anode & cathode coils	17
1.1.2. Mathematical Designing of Petersen Coils	20
1.2. Inserting of LTT Rectifying Thyristor Setting Circuit	24
1.3. Optimization of Mathematical Application	
for Damping Technique	24
1.3.1. Basic Module of Inductive Reactance Circuit	24
1.4. Synthesis of Mathematical Model	25
1.5. Synthesis of MATLAB/Simulink Models	26
1.6. Conclusions	28
 II. MATHEMATICAL PARAMETERS	 29
2.1. Experiment Test for Calculating of Oscillating – Chopping	
Currents – Proving Method	29
2.2. Experiment Prototype for Magnetic Field Behavior –	
Fabricated Process	31
 MAIN CONCLUSIONS	 32
BIBLIOGRAPHY	33

GENERAL DESCRIPTION OF THE WORK

Topicality

The main object of this research is a plan for designing and constructing of a new circuit breaker for medium voltage switching interrupter. In order to obtain soft interrupter, the following incidents are always happening inside the switching process: arcing currents, chopping currents and transient over voltages.

Beginning from the 18th century, all circuit breakers were filled with oil to prevent arcing currents, chopping currents and transient over voltages, which decomposed the dielectric material properties. In the beginning of the 20th century, all companies replaced the oily CBs by using new SF-6 Sulfur hexafluoride, non-flammable gas, to prevent explosion inside interrupter, but the success is still limited.

Technical engineering specification

Although most scholars, scientists and researching manufacturing companies are still confined in their efforts by using only a sustainable material such as copperchrome alloys “Metallurgy Vacuum Circuit Breaker” for protection against ionization and arcing currents, which are generated inside vacuum interrupter itself. However, the severe arcing currents, high scales of chopping currents may cause “accidental explosions” and are still registered in many factories and power generation plants.

In addition, static switching prototype creation still has many obstacles for a number of reasons: the automatic system is weakly developed, there are a lot of difficulties with the financial issue, because even the process of developing mathematical methods is difficult due to the many assumptions. The author of the Doctoral Thesis proposes a new technical solution by making a Petersen reactor coil for automatic adjustment – two coils with LTT thyristor set insertion in medium voltage switchgear [1]–[23] using MATLAB/Simulink.

Object of the Research

The object of research of the Thesis is the arc current and the chopping current occurring inside the vacuum interrupter. The aim of the Thesis is to use additional Petersen reactor coils for automatic adjustment of the switching process, as well as optimization of LTT thyristor set implementation for suppressing arc currents and chopping currents. In addition, the solution of the mathematical model synthesis problem obtains the result of static process modeling as a softswitching circuit breaker of a vacuum interrupter. Although there are three negative phenomena, mainly inside vacuum interrupter could be disruptive the insulation levels in medium voltage apparatus. However, there are also other disruptive phenomena, which are not so dangerous.

1. Restrikes of voltages – fast oscillating voltages.
2. Prestrikes over voltages – fast oscillating currents.
3. Multiple re ignitions.
4. Voltage escalation – oscillations phenomena.
5. Post-arc currents.
6. Thermal – Joule heating.

The author of the Thesis proposes a new invention, a softswitching circuit breaker, which completely eliminates arc current, chopping current and transient overvoltage.

Aim and Tasks of Research

The aim of my scientific work is to develop a methodology for creating the soft starting vacuum interrupter in medium voltage.

The author of the Thesis developed and adapted Petersen Reactor Coil Automatic Tuning for treatment of arcing currents “main obstacle”, including treatment of chopping currents and transient over voltages for second steps. Thus, the soft interrupter needs a new modification steps by optimization of mathematical Laplace formula and by creating a power electronics rectifying process for damping technique for automatic tuning.

For this purpose, one scholar created one sample “Harris model”.

Summarizing of Harris model switching interrupter was 600 μ s [1], [3], [5].

Table 1
Three MATLAB/Simulink/Design Samples Were Verified

Sample one	SION 3AES SIMENINES	63 A arcing current / 3 A chopping current for 12 kV
Sample two	SION 3AES SIMENINES	125 A arcing current / 5 A chopping current for 12 kV
Sample three	SION 3AE1 SIMENINES	250 A arcing current / 7 A chopping current for 12 kV

Tasks of the Thesis

1. To overview several research manuscripts on designing of damping applications that can be used in author's investigation for possibility of damping arcing currents (diffuse & constricted modes).
2. To develop the function of Petersen Reactor Coil Automatic Tuning, to design Anode Coil and Cathode Coil by applying the mathematical designing theory of designing Petersen application.
3. To develop recommendations for the Axel magnetic field utilization based on a prototype described in an international research paper data.
4. To carry out modeling experiments using synthesizing calculating method, in order to develop a calculation method to define the maximum values of chopping currents and to compare with the experiments (3 A / 5 A / 7 A) ABB carried out in Norway.
5. To define the objective function, to synthesize the necessary mathematical model/formula that will be used in optimization and inserting of LTT Thyristor set.
6. To optimize of the damping application method using MATLAB/Simulink software.

Applied Research Methods

The following research methods and means are used in this Thesis:

- qualitative research;
 - qualitative research on mathematical analysis for integration of power electronics in MV switching process with new LTT technique;
- new application of mathematical damping optimization technique;
- optimization of snubber circuit theory in MV application technique;
 - analysis of commutation process of di/dt in medium voltage switching;
 - damping of oscillating switching – MATLAB/Simulink experiment tests.

Scientific Novelty of Research

The used methods and the research allowed to achieve the following:

1. Two reactor coils (Anode Coil and Cathode Coil) were designed by developing the existing Peterson Reactor Coil Automatic Tuning in real time for the purpose of damping of arcing currents, chopping currents and transient over voltages to be the soft interrupter.
2. The steps of designing stages were done optimizing the mathematical application (synthesis of mathematical model) by inserting of LTT.
3. The results of the damping application used by Laplace transformation theory were presented in models in MATLAB.
4. The results that vacuum interrupter be able for working in the transition rate di/dt by a snubber power electronics process for shifting of the arcing currents and chopping currents precisely.
5. The MATLAB Invention is that the switching interrupter works as the sequential processing steps in uniform formula – (200 μs to 800 μs) between the electroplates.
6. The research proved that the snubber circuit in power electronics such as LTT thyristor type could be used.

7. The basic background steps of my research are based on doctoral theses by Mitchell, G. R and Harris, L. P. I made my research for quenching of arcing currents due to switching process inside vacuum interrupter itself.

Scientific and Practical Approbation of the Work

The research and its scientific novelty are scientifically approved in publications, conference proceedings and also practically approbated based on: Scientific Research Institute of Electrophysical Apparatus-Saint Petersburg whose constructed one sample reactor coil with thyristors auxiliary sets for charging and discharging application;

The Behlke Power Electronics LCC in Germany also constructed a one unit of LTT as Crowbar –snubber application (Behlke HTS 800-100-SCR) (11 kV / 150 kA) for parallel operating process, which is commercially available internationally and ABB (USA) research data

The research results have been presented in the following international conferences:

1. “Theoretical proved for synchronizing switching times of vacuum Interrupter with power electronics – Thyristor for the same transition rates between electroplates and thyristor for medium voltage switching system”. *Third International conference on artificial intelligence Lodz university of technology; Lodz-Poland, September 2016.*
2. “Analysis of parameters and time sequences for full operation mode of vacuum Interrupter for medium voltage switching system”. *52nd International scientific conference on information, communication and energy system (ICEST 2017) Niš, Serbia, June 28–30, 2017.*
3. “Analysis of parameters of transient over-voltages and measuring of chopping currents on vacuum Interrupters associated with medium voltage switching system”. *52nd International scientific conference on information, communication and energy system (ICEST 2017) Niš, Serbia, June 28–30, 2017.*

Innovations

For some of the research results the following patents have been registered:

1. Flexibility of transition materials di/dt & du/dt criteria, a mathematical model was constructed by two scientists Glinkowski and Greenwood proved of the switching electroplates ($50 \text{ A}/\mu\text{s} < di/dt < 1250 \text{ A}/\mu\text{s}$) that was supporting author researching for studying a parallel operation mode, between electroplates and semiconductor materials, 11 kV In MATABL/Simulink experiment tests.
The main purpose for proved of manuscript that enhanced the using of crowbar application, basically for the process of Peterson Reactor Coil (0093-9994/03\$17.00@2003IEEE).
2. The mathematical formula of Harris model enables author fabricating the existing of Peterson coil automatic tuning in real time 600 μs of Inductive reactance ωL value of 11 kV at rate of $I_c = 250 \text{ A}$ in damping application techniques for oscillating chopping currents and transient over voltages in vacuum interrupter by using of Laplace theory including implementing by MATLAB.
3. These data sheet was assumed the maximum arcing current (12 kV/ 250 A) for my designing novelty and author researching proved at three values of chopping current (3 A/ 5 A/ 7 A).
4. IEEE tutorial on the vacuum switchgear “ TP-135-0” confirmed that *“when the current chopped inside vacuum, its causes the changing in the frequency values 50 Hz to 150 Hz and 400 Hz”* this phenomenon invited me to study the mathematical behaviors. Author interpretation is that *“there is an interval in phenomena among arcing current, chopping current and transient over voltages come together to generate switching impulses in primitive mode inside interrupter”* this patent according to the Fourier series phenomena in more detail is explained by Erwin Kreyszig the Advanced Engineering Mathematics & MATLAB /Simulink application.

Author's publications

Researches carried out in this dissertation have been presented in the following publications:

1. "The Modern Methods for Designing of Medium Voltage Switchboards Technology of Power Plant's Refineries," Proceedings of the IEEE 3rd workshop on advances in information, Electronic and Electrical Engineering (AIEEE), Riga Technical University, Riga, Latvia, 2015. ISSN 978-1-5090-1201-5.
<https://doi.org/10.1109/aieee.2015.7367284>.
2. "Synchronizing Switching Times of Vacuum Interrupters for Medium Voltage – Switchboards' Techniques," Proceedings of the IEEE 3rd International conference on artificial intelligence (AIPR 2016), University of Technology – Lodz, Poland Lodz, 2016. ISBN 978-1-4673-9187-0.
<https://doi.org/10.1109/icaipr.2016.7585204>.
3. "Algorithmic Application for Calculation of chopping Currents and High Transient over-voltages for a New Vacuum Interrupter," 2017 International Scientific Conference on Information, Communication and Energy Systems and Technologies (ICEST 2017), University of Nis Serbia. ISSN 2603-3259.
4. "Analyzing Parameters of Load Flows and Characteristics of Medium Voltage Switching System – Refinery Power Plant," 2017 International Scientific Conference on Information, Communication and Energy Systems and Technologies (ICEST 2017), University of Nis Serbia. ISSN 2603-3259.
5. "A New Method for Parallel Operation Units by Synchronized Instrument Transformers –Associated with Switchboards P1," 2017 International Scientific Conference on Information, Communication and Energy Systems and Technologies (ICEST 2017), University of Nis Serbia, 2017. ISSN 2603-3259.
6. "A New Method for Parallel Operation Instrument Transformers Units by – Associated with Switchboards," 2017 IEEE 58th International Scientific Conference on Power and Electrical Engineering of Riga Technical University (RTUCON), Okt. 2017. <https://doi.org/10.1109/rtucon.2017.8125623>.

7. "Analysis of Parameters and Time Sequences for Full Operation Mode of Vacuum Interrupter for Medium Voltage Power Plants," *American Journal of Information Science and Technology*, vol. 2, no. 2, 2018, pp. 57–63.
<https://doi.org/10.11648/j.ajist.20180202.15>.

STRUCTURE OF THE WORK

1. Medium Voltage Switching Parameters

- 1.1 Switching parameters
- 1.2 Switching characteristics and multiple voltage escalation
- 1.3 Capacitive current Interrupter
- 1.4 Inductive current Interrupter
- 1.5 Experiment test one – Transition Rate of di/dt
- 1.6 Experiment test two – Formation of Radial Magnetic Field
- 1.7 Conclusions

2. Contacting Materials of M.V Switching

- 2.1 Analysis of technical materials inside vacuum interrupter
- 2.2 Types of vacuum arcs
- 2.3 Calculating of Joule heating in vacuum interrupter
- 2.4 Synthesis of mathematical model
- 2.5 Electrode effects and break- down
- 2.6 Transient over voltages formula
- 2.7 Mathematical Fourier transformation model
- 2.8 Experiment test for calculating of chopping currents
- 2.9 Calculating of NSD discharging times – Experiment Test
- 2.10 onclusions

3. Design Circuit & Mathematical Applications

- 1.1 Hypothesis of static vacuum Interrupter
 - 3.1.1 Analysis of the designing of the existing Petersen Coil Automatic Tuning
 - 3.1.2 Fabricating of Petersen Coil -Anode Coil & Cathode Coil
 - 3.1.3 Inserting of LTT rectifying Circuit
 - 3.1.4 Synthesis of mathematical model
 - 3.1.5 Synthesis of MATLAB/Simulink models

Main conclusions

Appendices

Appendix 1 – Damping Mathematical Application -Example

Appendix 2 – Splitting of Arcing Currents – Power Electronics – Experiment Tests

Appendix 3 – Pulse Power Equipment by LTT Thyristor

Appendix 4 – Transition of Switching Rates du/dt & di/dt on Snubber Application

DISSERTATION BRIEFLY

In order to get better understanding of my research term specifically. It depends on the existing of the industrial manuscripts, which involve medium voltage interrupter process as a standard, even if that was publishing dates because the valuable samples were really reflected in scientific information. So, we shall confine our attention mainly on only the above three measurements: arcing currents, chopping currents and transient over voltages.

G.R. Mitchell classified two types of arcing currents:

1. Diffuse Mode.
2. Constricted Mode.

In addition, there are two elements that could be made a disruptive of the dielectric insulation levels; chopping currents and transient over voltages.

My investigation confirmed that there is an intervene between chopping currents events and transient over voltages when they come together and initiate a high escalation of switching impulses in a primitive mode (first invention step).

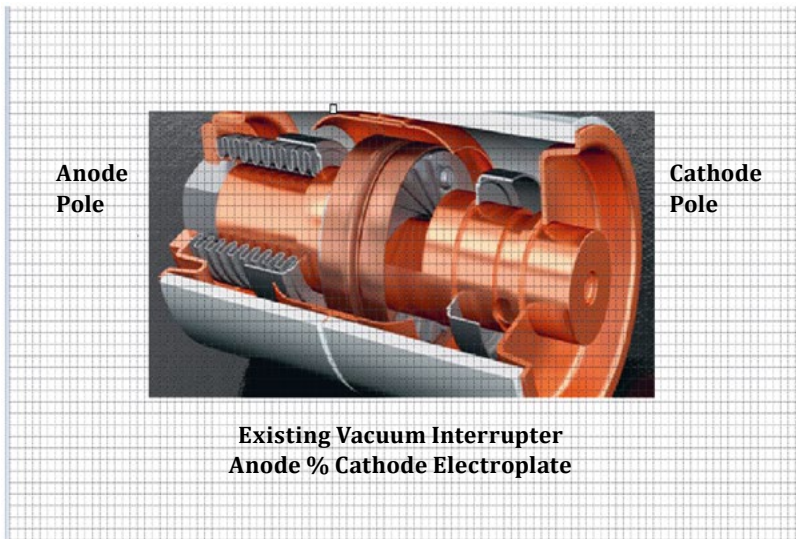


Fig. 1.1. The existing vacuum interrupter under investigation.

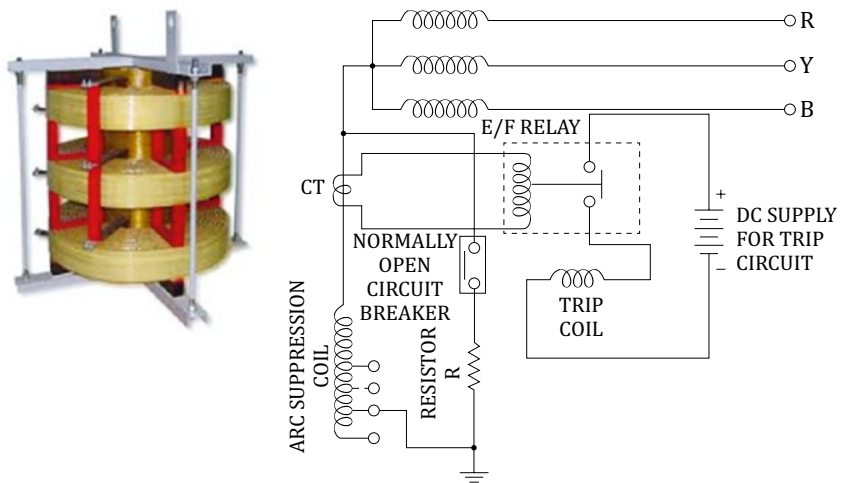


Fig. 1.2. Petersen reactor coils automatic tuning under research.

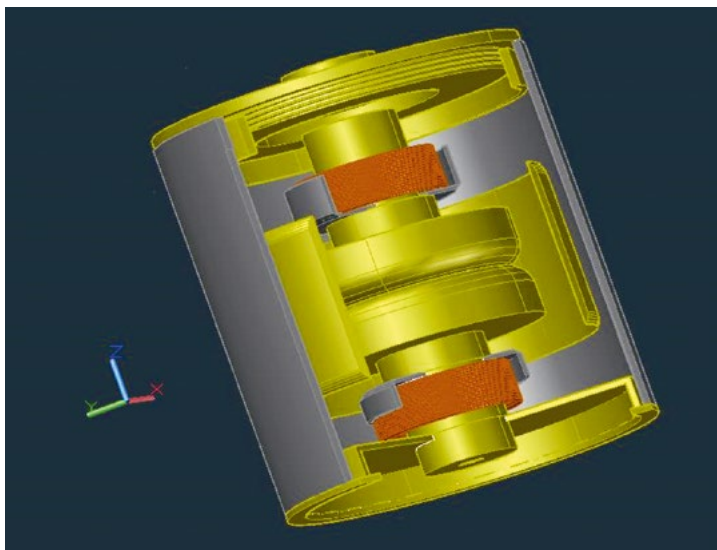


Fig. 1.3. Fabricated Petersen coils – anode and cathode poles. Sample 1.

I. FABRICATING AND DESIGNING

1. HYPOTHESIS OF STATIC VACUUM INTERRUPTER

My Thesis proposed that created damping processes unit for occurrence of the soft starting interrupter has the following steps:

1. Hypothesis of static vacuum interrupter.
 - 1.1 Designing, fabricating and modifying of the Petersen Reactor Coils Automatic Tuning.
 - 1.1.1 Fabricating Anode & Cathode Coils.
 - 1.1.2 Mathematical designing of Petersen coils.
 - 1.2 Inserting of LTT rectifying thyristor setting circuit.
 - 1.3 Optimization of mathematical application for damping technique.
 - 1.4 Synthesis of mathematical model.
 - 1.5 Synthesis of MATLAB/Simulink models.
 - 1.6 Conclusions.
2. Experiment test and samples.
 - 2.1 Experiment test for calculating of oscillating-chopping currents.
 - 2.2 Experiment prototype for magnetic field behavior.
 - 2.3 Fast-discharging unit – prototype – Russian Institute.

Main conclusions.

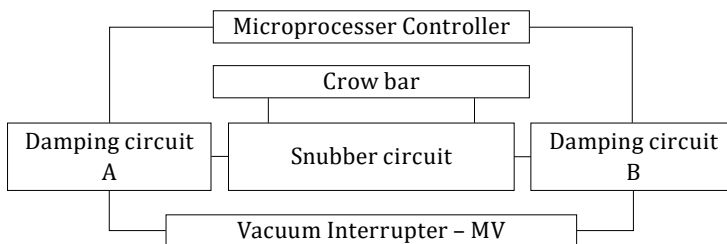


Fig. 1.4. Single Line diagram of vacuum interrupter under investigation (novelty).

1.1. Designing, Fabricating and Modifying of the Petersen Reactor Coils Automatic Tuning

Petersen coils are used in faults of 3-phase systems to limit arcing currents during earth faults process. The coil was first developed by William Petersen and still installed in all substations. However, the use of modern power electronics has revolutionized the performance of these classical solutions called Arc Suppression Coil (ASC) and the modern power electronics have been offered a new automatic tuning technique. My second invention was fabricated in order for this reactor to be more convenient in each pole of interrupter [1], [7], [18].

1.1.1. Fabricating Anode & Cathode Coils

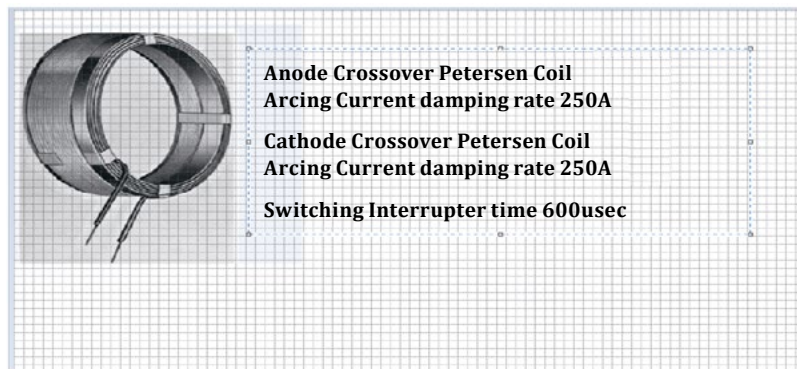


Fig. 1.5. Preliminary designing of fabricated Petersen coil.

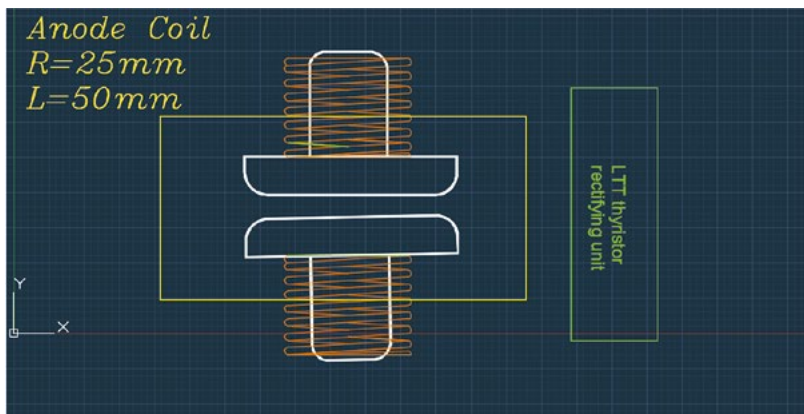


Fig. 1.6. Preliminary designing of fabricated Petersen coil with LTT thyristor (proposed novelty).

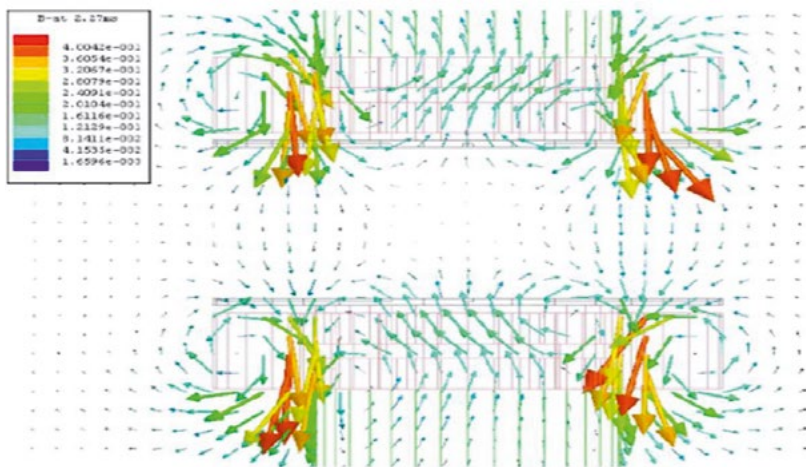


Fig. 1.7. AMF rotates between anode and cathode Petersen coils [27].

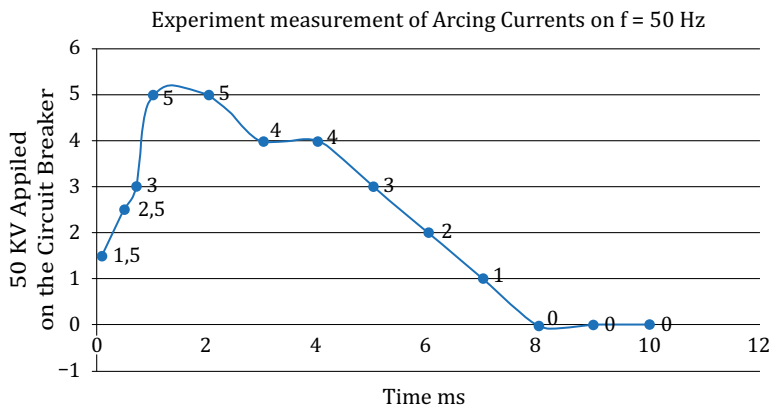


Fig. 1.8. Maximum arcing currents – experiment MATLAB test.

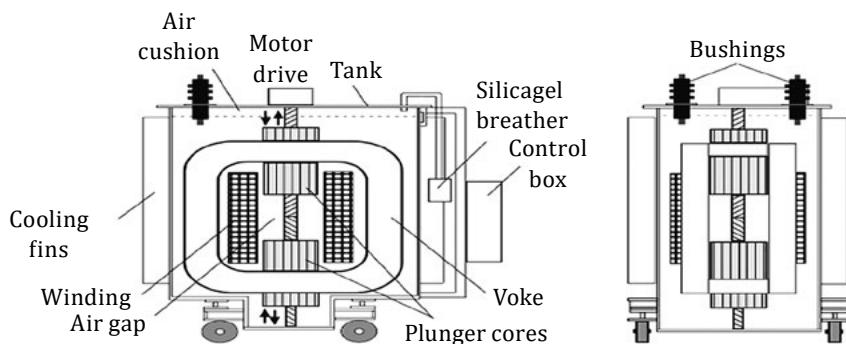


Fig. 1.9. Construction diagram of Petersen reactor coil automatic tuning.

Researching for fabricating of axial magnetic field.

- Quenching of arcing currents.
- Quenching of chopping currents.
- Preventing of initiate transient over voltages.
- Analysis of Petersen two coils – primary windings – secondary windings with moving of secondary coil tap changer automatic tuning principle.
- $U = 12$ kV.
- $I = 70$ kA.

- $U_d = 28$ kV Minimum switching impulse.
- $U_p = 75$ kV Maximum switching impulse.
- Quenching arcing currents – 250 A at maximum frequency range [50 Hz to 150 Hz / 400 Hz].
- Maximum time switching of arcing currents [0–600 μ s].
- Maximum discharging technique of [Coil A – THY – Coil B].
- Insulation level U_d (kV rms. 1 min) and U_p (kV peak).
- LTT Thyristors – Lighted Triggered Power Switching [21].

1.1.2. Mathematical Designing of Petersen Coils

For designing of Petersen coil automatic tuning for the function of quenching both of arcing currents and chopping currents, it is customary to assume that the highest allowable current is produced at the arc suppression value. Upon this basis the following formula for the ohmic value. The current limiting coil should be considered of a resistor, an inductor, a capacitor or any combination of these.

$$I = \frac{1000S}{U\sqrt{3}}, \quad (1.1)$$

$$Z_p = \frac{U}{\sqrt{3}C_o \cdot I}, \quad (1.2)$$

where

Z_p – impedance for anode & cathode coils, Ω ;

I – maximum current passing in coil, amperes, A;

U – transformer turned line volts 12 kV;

S – winding of transformer coil, kVA;

C_o – coefficient of arcing currents & chopping currents.

So, the designing formula for anode and cathode coils is as follows:

$$Z_p = \frac{U^2}{2000C_o \cdot S} \text{ (for single pole of interrupter),} \quad (1.3)$$

$$L = \frac{1}{3\omega c}. \quad (1.4)$$

Sample 1: $L = 16 \text{ mH}$ for $Z = 32.699 \Omega$ (anode & cathode coils)

$Z_p = 32.00 \Omega$ for anode winding coil – 1.1 mm cross section copper wire.

$Z_p = 32.00 \Omega$ for cathode winding coil – 1.1 mm cross section copper wire.

LTT/THY rating 63 A / 12 kV / 1200 $\mu\text{s/A}$ 180 kA / LTT type.

Dimension of anode & cathode coils:

- $R = 25 \text{ mm}$;
- $L = 50 \text{ mm}$.

Pole diameter = 125 mm standard on the existing vacuum interrupter type SION / 3AES SIMENS 12 kV / 630 A.

- My novelty confirms that the axial magnetic field shall rotate in the first coil – anode coil.
- For the purpose of process to diverting of three elements outside electroplates.

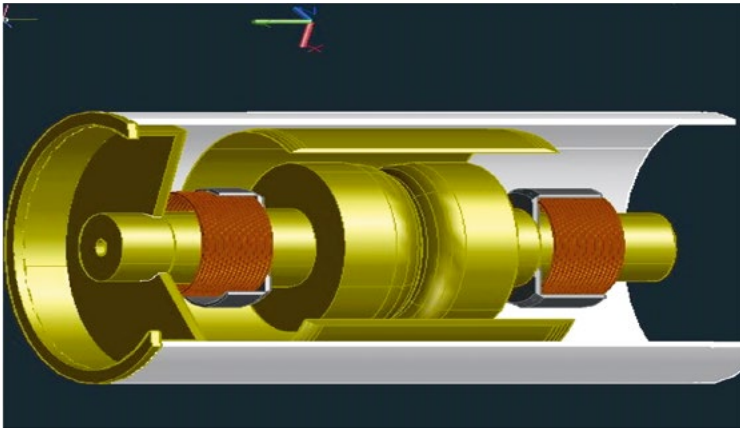


Fig. 1.10. Designing of Petersen reactor coil automatic tuning anode & cathode. Sample 1.

Sample 2: $L = 20 \text{ mH}$ for $Z = 50.24 \ \Omega$ (anode & cathode coils)

$Z_p = 50 \ \Omega$ for anode winding coil – 1.55 mm cross section.

$Z_p = 50 \ \Omega$ for cathode winding coil – 1.55 mm cross section.

THY Rating 125 A / 12 kV / 1200 $\mu\text{s/A}$ 180 kA / LTT.

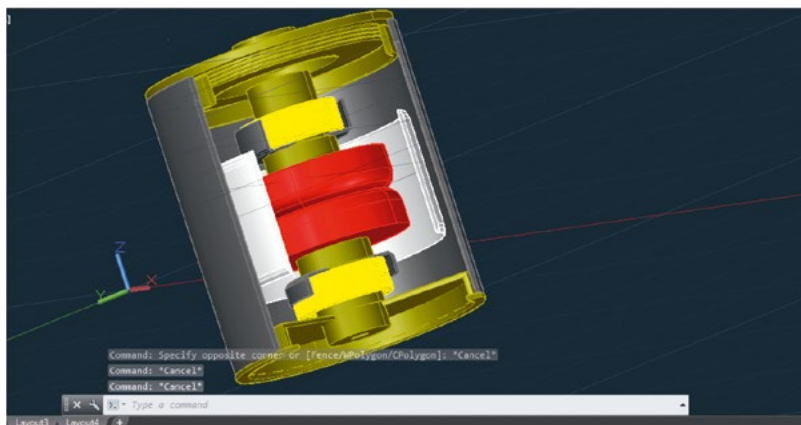


Fig. 1.11. Designing of Petersen reactor coil automatic tuning anode & cathode. Sample 2.

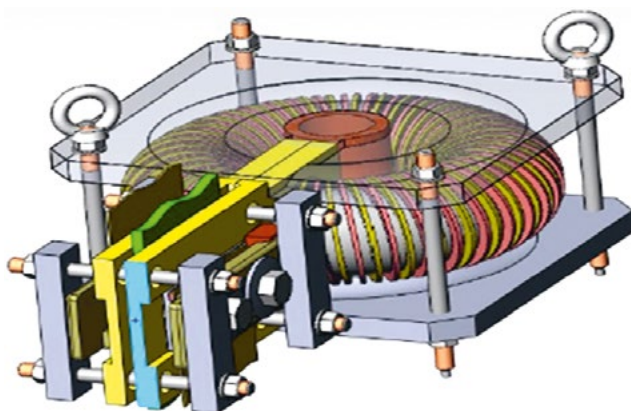


Fig. 1.12. Modification sample of anode & cathode poles.
Sample – St Petersburg Institute.

- RTU does not have M.V. laboratory
- My analysis for finding similar scientific materials of my novelty.

Sample 3: $L = 40 \text{ mH}$ for $Z = 63.49 \Omega$ (anode & cathode coils)

$Z_p = 63 \Omega$ for anode winding coil – 1.75 mm cross section.

$Z_p = 63 \Omega$ for cathode winding coil – 1.75 mm cross section.

THY Rating 250 A / 12 kV / 1200 $\mu\text{s/A}$ 180 kA / LTT.

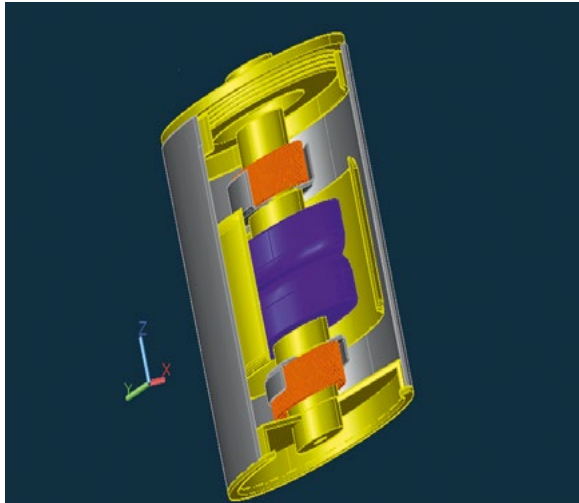


Fig. 1.13. Designing of Petersen reactor coil automatic tuning anode & cathode. Sample 3.

1.2. Inserting of LTT Rectifying Thyristor Setting Circuit

One concluding theory from a group of Scholars [64]:

$$I_0 = i_1 + i_2. \quad (1.5)$$

$$U_1 + L_1 \frac{di_1}{dt} = U_2 + L_2 \frac{di_2}{dt}. \quad (1.6)$$

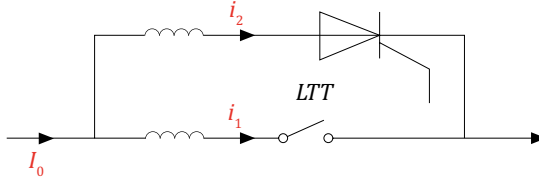


Fig. 1.14. The switching on LTT will be crossing speed by Kirchhoff's law.

1.3. Optimization of Mathematical Application for Damping Technique

In order to create mathematical formula, which is being more facility for damping application of two coils (Anode Coil A & Cathode Coil B) in parallel operation including one thyristor set for soft interrupter, we shall design basic module of inductive reactance value of 20 mH for my Thesis of proposed circuit [11], [21].

1.3.1. Basic Module of Inductive Reactance Circuit

$$e^{at} t^n = \frac{n!}{(s-a)^{n+1}}. \quad (1.7)$$

Damping real part:

$$e^{at} \cos(\omega t) = \frac{(s-a)}{(s-a)^2 + \omega^2}. \quad (1.8)$$

Damping imaginary part:

$$e^{at} \sin(\omega t) = \frac{\omega}{(s-a)^2 + \omega^2}. \quad (1.9)$$

In this case of rectifying both of arcing currents and chopping currents $I_p = I_{arc} + I_{ch}$.

$$I_p = \sqrt{\frac{1}{2\pi} \int_0^\pi I^2 d(\omega t)} =$$

$$= \sqrt{\frac{I_m^2}{2\pi} \int_0^\pi \sin^2(\omega t) d(\omega t)} = \frac{I_m}{2}. \quad (1.10)$$

rectifying values of arcing currents and chopping currents

1.4. Synthesis of Mathematical Model

1. The main benefit of the fabricated Petersen coil is that the axial magnetic field will be rotated as radial magnetic field when passing the sealing vacuum tube in each pole. This phenomenon is very important that arcing currents will not growth escalation from the rate of arc suppression coil. This my application technique was verified by the research manuscript [5].

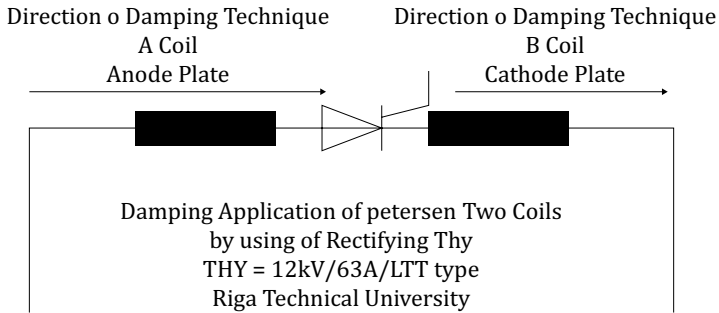


Fig. 1.15. Mathematical model – basic module circuit for rectifying application (novelty).

2. The designing of winding coils was verifying the equation (1.1) for calculating of the maximum both of arcing currents and chopping currents.
3. LTT Thyristor were chosen from the data sheets – specification [95].

1.5. Synthesis of MATLAB/Simulink Models

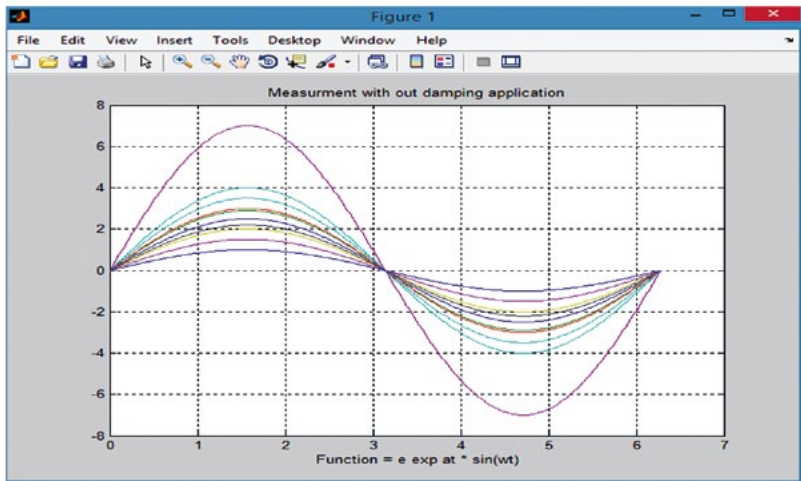


Fig. 1.16. Basic module circuit without damping application – MATLAB.

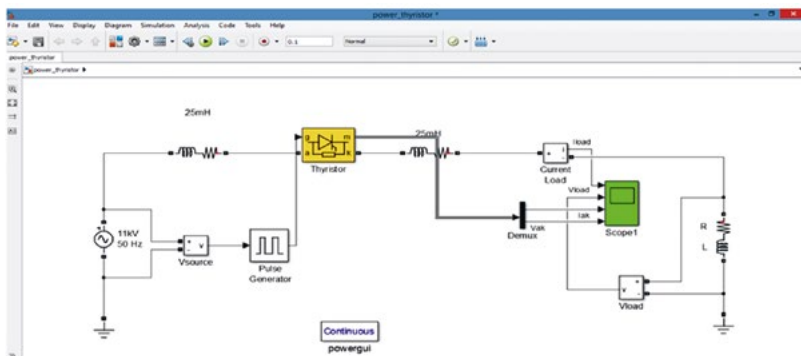


Fig. 1.17. MATLAB/Simulink Basic Module.

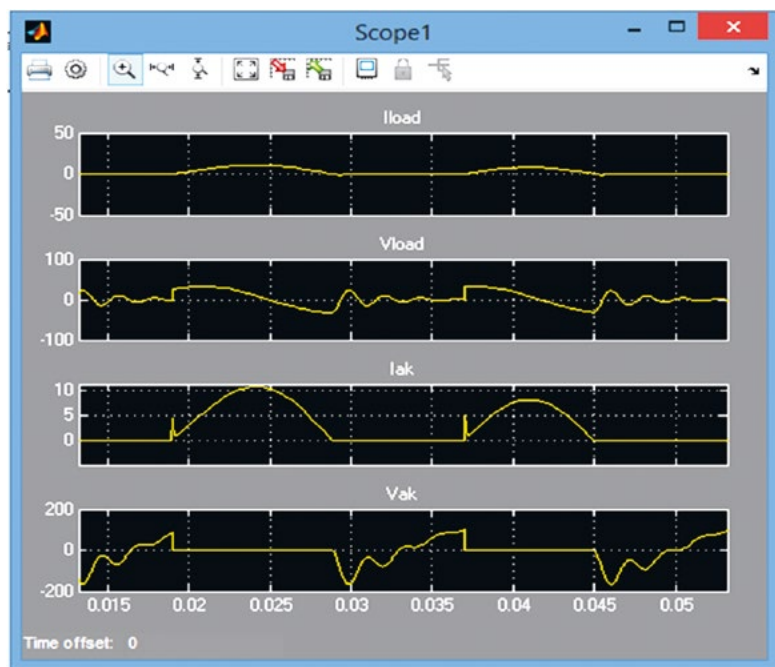


Fig. 1.18. MATLAB/Simulink Basic current.

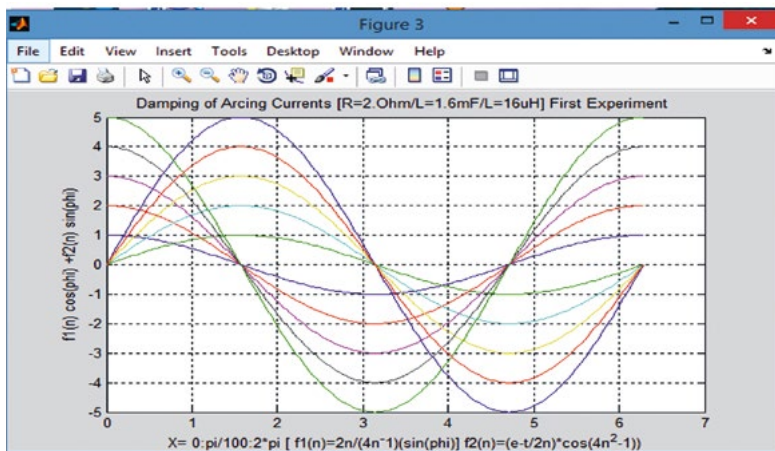


Fig. 1.19. Generalized plot of Laplace transformation – damping circuit – MATLAB.

1.6. Conclusions

Allan Greenwoods and his colleagues were creating a mathematical method for created damping general formula. My development that was made some experiment tests by using MATLAB/Simulink for clarifying the benefit of the mathematical application damping rectifying technique [6], [11], [12].

$$i_{L(s)} = \frac{U_{(0)}}{L} \cdot \frac{1}{\left(S^2 + \frac{s}{TP} + \frac{1}{T^2}\right)}, \quad (1.11)$$

whereas

$$LC = T^2.$$

Mathematical parameters for theory of damping circuits:

$$\frac{U_{\text{out}}}{U_{\text{in}}} = \frac{1}{LS^2 + RS + 1}, \quad (1.12)$$

$$\frac{C_{(s)}}{R_{(s)}} = \frac{1}{\left(S^2 + 2\xi_s + 1\right)}.$$

To determine the first overshoot at T_{max} ,

$$T_{\text{max}} = \frac{n\pi}{\omega_n \sqrt{1 - \zeta^2}}. \quad (1.13)$$

In order to generate calculating parameters for designing (L) reactor which is able to damping all transient over voltages, there are three requirements that need to be considered, precisely f_1 , f_2 and f_3 .

$$f = \frac{1}{2\pi\sqrt{LC}}. \quad (1.14)$$

II. MATHEMATICAL PARAMETERS

2.1. Experiment Test for Calculating of Oscillating – Chopping Currents – Proving Method

Calculating of the first peak value of chopping currents and evaluate the transient over voltages on Petersen Coil Reactor Transformer was verified on one reactor coil with ABB laboratory in Drammen, Norway [10].

$$\begin{aligned} Z_{\text{Load}} &= 3000 \, \Omega, \\ U_T &= I_{\text{ch}} Z_{\text{Load}}, \end{aligned} \quad (2.1.)$$

where

U_T – voltage of the first peak value;

I_{ch} – current chopping;

Z_{Load} – load impedance.

In order to verify the statistical approach of the correctly calculation of first peak values for each circuit breaker $U_T = 0.9 \cdot 3000 = 2700 \, \text{V}$ first peak transient voltage.

$U_{\text{MAX}} = 2.7 \, \text{kV} + 10 \, \text{kV} = 12.7 \, \text{kV}$ reasonable transient over-voltage. Thus the table indicates the data sheet regarding my calculation permissible for full operation loads.

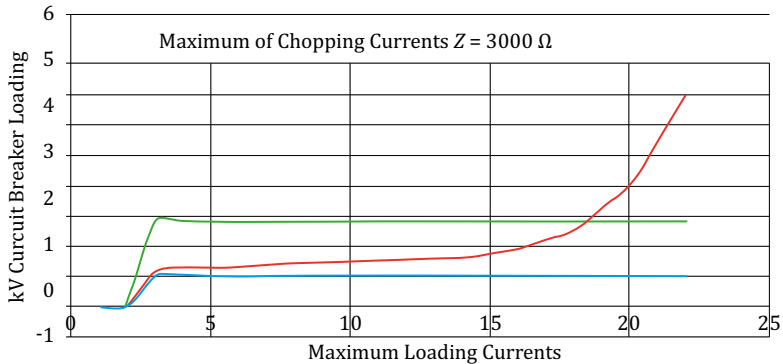


Fig. 2.1. Data sheet for finding maximum chopping currents.

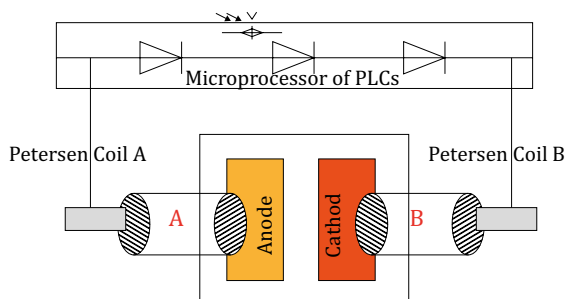
Table 2.1
Calculating Chopping Currents and Transient Over
Voltages – $Z = 3000 \, \Omega$

No	I_c, A	U_T, kV	U, kV	U_{max}, kV	U_d, kV	Results
1	0.1	0.3	10	10.3	28	Acceptable
2	0.2	0.6	10	10.6	28	Acceptable
3	0.3	0.9	10	10.9	28	Acceptable
4	0.5	1.5	10	11.5	28	Acceptable
5	0.9	1.7	10	12.7	28	Acceptable
6	1	3	10	13	28	Acceptable
7	2	6	10	16	28	Acceptable
8	3	9	10	19	28	Acceptable
9	4	12	10	22	28	Acceptable
10	5	15	10	25	28	Critical
11	6	18	10	28	28	Critical
12	7	21	10	31	28	Disruptive
13	8	24	10	34	28	Disruptive
14	9	27	10	37	28	Disruptive
15	10	30	10	40	28	Disruptive

2.2. Experiment Prototype for Magnetic Field Behavior – Fabricated Process

Table 2.2
Experiment Indicates the Fixed Arcing Currents Value

Number	Time ms	Arcing Voltage KV	Peak Value KA	Results
1	0	0	0	$i = I_m \sin \omega t$
2	1,5	10	13,7	Pārsniegts
3	1,9	20	15,5	Pārsniegts
4	2,0	25	17,0	Pārsniegts
5	2,0	30	14,1	Stabils
6	2,5	35	14,0	Stabils
7	3,0	40	13,0	Samazināts
8	3,0	45	12,0	Samazināts
9	3,5	50	12,0	Stabils
10	3,5	55	12,0	Stabils
11	4,0	60	12,0	Stabils



Preliminary designing of two coils for soft starter
11 kV / 250 A / 600 μ s / 25 mH
Vacuum Interrupter auxiliary circuit

Fig. 2.2. Preliminary designing of soft starter unit (novelty).

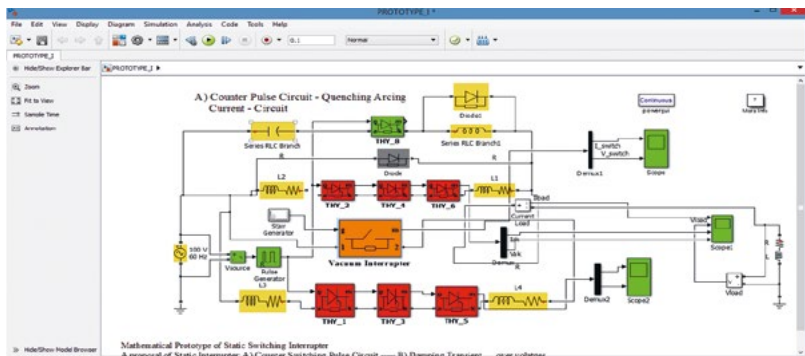


Fig. 2.3. MATLAB/Simulink – soft starter unit of vacuum interrupter.

MAIN CONCLUSIONS

1. The author proposes an automatic adjustment of Petersen reactor coils: the dual-winding coils have improved damping of both the arc current and the chopping current with a soft switching circuit breaker, which offers a switching pulse correction process.
2. The MATLAB method proposed by the author provides optimized calculation of the corrective LTT switching for a 12 kV / 63 A / 3 A set of 12 kV / 125 A / 5 A and 12 kV / 250 A / 7 A.
3. The developed process that describes the sequential modeling process for a softswitching of circuit breaker.
4. The result of the author's development is a switching process of up to 600 μ s.
5. The author concludes that static discharge switching times do not affect the switching process.
6. The author proposes the use of softswitching circuit breakers with two Petersen coils as a new technology in medium voltage networks.

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